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# Effects of $CO_2$ and steam on Ba/Ce-based $NO_x$ storage reduction catalysts during lean aging

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#### ABSTRACT

The effects of  $CO_2$  and steam on the morphological and chemical properties of Ba/Ce-based  $NO_x$  storage reduction (NSR) catalysts during the aging were investigated. At 800 °C,  $BaCeO_3$  formation was prevented by a  $CO_2$  concentration as low as 5%, which shows little effect on suppressing  $BaAl_2O_4$  and  $BaZrO_3$  formation.  $CO_2$  protects hexagonal  $BaCO_3$ ,  $BaO_2$ , and  $CeO_2$ , to form  $BaCeO_3$ , by increasing one time higher activation energy for decarbonation, and maintaining orthorhombic  $BaCO_3$  as the most stable storage component. Steam accelerates the particle aggregations, but it does not determine the above chemical equilibrium. In NSR reactions, although  $BaCeO_3$  formation can be excluded in an atmosphere containing  $CO_2$ , the nitrite/nitrate bonding stabilization and the complete  $NO_x$  reduction are hindered by the highly crystallized materials (induced by higher  $CO_2$  and/or steam concentrations during aging). Particle aggregation is a major factor responsible for the deactivation of the aged Ba/Ce-based NSR catalysts.

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# 1. Introduction

Lean  $NO_x$  trap (LNT), also known as  $NO_x$  storage reduction (NSR), has drawn wide attention as an advanced exhaust control technology to reduce  $NO_x$  emissions from lean-burn engines [1]. A typical NSR catalyst formulation contains basic  $NO_x$  storage components (mostly barium species), noble metals (NM, such as Pt, Rh, Pd), and support oxides. The combined effects of these three components efficiently remove  $NO_x$  from vehicle exhaust through the periodic operations of  $NO_x$  oxidation,  $NO_x$  sorption,  $NO_x$  release, and  $NO_x$  reduction [2,3].

Ceria-based materials have been shown to be beneficial for NSR catalysts. They maintain higher metal dispersions [4], provide surface basicity to benefit the formation of carbonates [5], promote the water–gas shift (WGS) reaction and the reduction of  $NO_x$  at anionic vacancies [6], and release lattice oxygen, which modifies the redox process [7]. Many current commercial samples have already incorporated ceria into  $NO_x$  traps. Several research articles have reported the outstanding performance of Ba/Ce-based NSR catalysts compared to the catalysts with other oxide supports (Al, Si, or

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Zr), although ceria-based materials are admitted to have several drawbacks [3,8,9]. Not only do ceria-based materials sinter at relatively low temperatures [3], they also maintain the oxidation states of NM during rich periods [10], and their surface basicity is negative for NO oxidation in lean conditions [11].

Thermal deterioration, especially with concern to the modification of NO<sub>x</sub> storage components [12], is one of the main reasons for the deactivation of NSR catalysts [2]. Besides several recent studies focused on the Pt-Ba interactions [13,14], much emphasis is put on the barium-based components modified by the Ba-support interactions [2,3]. The formation of BaCeO<sub>3</sub>, BaAl<sub>2</sub>O<sub>4</sub>, and BaZrO<sub>3</sub> in Ba/Ce, Ba/Al, and Ba/Zr systems is well documented, and these compounds are known to decrease the NO<sub>x</sub> storage efficiency [9,15]. Additionally, investigations into the regeneration of thermal-aged NSR catalysts have been reported [12,15]. In general, treatments in an acidic liquid (water) or a 300-800 °C acidic atmosphere, in which H<sub>2</sub>O, NO<sub>x</sub>, and CO<sub>2</sub> are applied at concentrations much higher than those in the exhaust, are required for the regenerations. Therefore, it is desirable to develop a heterogeneous NSR catalyst that does not form the inactive phases during the aging treatment or readily regenerates the deactivated phases under realistic conditions in vehicle exhaust [2]. Regeneration of BaCeO<sub>3</sub> is more likely when compared with that of BaAl<sub>2</sub>O<sub>4</sub> and BaZrO<sub>3</sub> [15]. However, the possibility of BaCeO<sub>3</sub> formation under realistic applications was questioned due to the lower concentrations of CO<sub>2</sub> and H<sub>2</sub>O

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**Table 1**Descriptions of the different aging treatments.

	•					
	Names of the treatments	Brief description (for 0–18 h aging)				
tr Fr Tl H; 59 10	Fresh Thermal Hydrothermal 5% CO <sub>2</sub> thermal 10% CO <sub>2</sub> thermal 5% CO <sub>2</sub> hydrothermal 10% CO <sub>2</sub> hydrothermal	As-prepared samples Samples treated in 800 °C air Samples treated at 800 °C in 10% steam (air balance) Samples treated at 800 °C in 5% CO <sub>2</sub> (air balance) Samples treated at 800 °C in 10% CO <sub>2</sub> (air balance) Samples treated at 800 °C in 5% CO <sub>2</sub> + 10% steam (air balance) Samples treated at 800 °C in 10% CO <sub>2</sub> + 10% steam (air balance)				

<sup>\*</sup> All percentages presented stand for gaseous percentages in volume.

(NO<sub>x</sub> can be eliminated) found in lean-burn exhaust [12]. It is not clear whether the decent activity of Ba/Ce-based NSR catalysts is due to the higher NO<sub>x</sub> storage capacity (NSC) of BaCeO<sub>3</sub>, or the improved maintenance of active phases against BaCeO<sub>3</sub>.

The performance of the aged NSR catalysts strongly depends on the real operation conditions; and therefore, the lab aging strategies should be careful examined. Even at similar temperatures, different atmospheric compositions during the aging treatments will have a significant impact on the aged catalyst performance [5,16]. In contrast to the periodically varying  $NO_x$  concentrations (eliminated at most of the time), the concentrations of  $CO_2$  and steam are kept almost at a constant level during the lean–rich cycles. Their continuous effects of modifying NSR materials should be studied.

Temperature-dependent effects of steam and CO<sub>2</sub> during NSR reactions have been systematically studied [5,16], but their influences during long time aging have yet to be thoroughly investigated. In the present work, the effects of CO<sub>2</sub> and steam on the morphological and chemical properties of Ba/Ce-based NO<sub>x</sub> NSR materials during the aging treatments were studied through surface/bulk analysis and activity tests. Since there is little evidence that noble metals change the Ba-support interaction [13,17], the NM-related interactions have been decoupled from the Ba-Ce contact for most of the samples we investigated.

# 2. Experimental

# 2.1. Sample preparation

For the supported samples, Pt and BaO were loaded by wet impregnation, using Pt(NO<sub>3</sub>)<sub>2</sub> and Ba(Ac)<sub>2</sub> solutions, respectively. CeO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, and ZrO<sub>2</sub> support oxides were from Aldrich. The impregnated materials were calcined in air at 500 °C for 5 h to obtain the fresh samples. Only the BaO/CeO<sub>2</sub> parts were treated under different aging conditions, and they were mixed with the fresh 2 wt.% Pt/Al<sub>2</sub>O<sub>3</sub> in the weight ratio of 6:4 right before the catalytic tests. For comparison, 2 wt.% Pt/30 wt.% BaO/CeO<sub>2</sub> samples and 30 wt.% BaO/2 wt.% Pt/CeO<sub>2</sub> samples were also prepared (Pt and Ba impregnated with reverse sequences), in which the NM and barium species were loaded on the same support oxide in reverse sequences. Descriptions of the different treating strategies are listed in Table 1.

Pertaining to the impregnated BaO/CeO<sub>2</sub> samples, the contact between barium species and ceria takes place on the interface where the barium salts were wet-impregnated. According to our X-ray diffraction and thermogravimetric data, the insufficient close Ba–Ce contact and less barium content make the quantification of the major phases and the tracking of the minor intermediate species difficult. Therefore, co-precipitated Ba/Ce (molar ratio 1:1) mixed compounds magnifying the Ba–Ce close contact, designated as BaCe11, were used in the study for comparison. The BaCe11

samples were prepared by adding  $Ce(NO_3)_3 \cdot 6H_2O$  and  $Ba(NO_3)_3$  into a  $NH_4HCO_3$  precipitator. Additional basic solutions were added until pH = 9 (200% in excess). The precipitates were stirred at room temperature (RT) for 30 minutes and stabilized at 60 °C for 12 h. After being filtered and washed with de-ionized water till pH = 7, the products were dried at 100 °C for 12 h. Fresh powders were obtained after the subsequent calcination in air at 500 °C for 5 h. The majority of fresh powder is able to be converted into BaCeO<sub>3</sub> crystallites after 4 h calcination at 1100 °C according to XRD analysis [18,19].

# 2.2. Characterization and model reaction

The XRD patterns were acquired using X'Pert Pro diffractometer operating at 30 kV and 30 mA with nickel-filtered Co K $\alpha$  radiation, at a 0.02° step size. For *in situ* experiments, the heating rate from RT to the target temperature was 10 °C/min, and the space velocity was  $10,000\ h^{-1}$ . Percentages of detected crystallites in samples were estimated by comparing the obtained XRD patterns with the monocomponents patterns of standardized crystallites in HIGHSCORE software database. Crystal sizes are calculated by JADE 5. Thermogravimetric experiments were conducted on METTLER TOLEDO TGA/DSC 1. Approximately, 20 mg of fresh sample was heated in a gas flow (50 ml/min) at a heating rate of 5, 10, and 15 °C/min, respectively.

BET surface areas were measured using  $N_2$  adsorption with a Quantachrome NOVA 1200. Scanning electron microscopy (SEM) of the samples coated with Au–Pd was measured on a HITACHI S4800 field emission microscope. X-ray energy dispersive spectroscopy (EDS, NORAN System 7) results indicated that the enrichment of BaCO<sub>3</sub> generally shows deep color,  $CeO_2$  the intermediate, and BaCeO<sub>3</sub> the light color.

In situ DRIFTS of  $NO_x$  isothermal adsorption and temperature programmed desorption were performed on a NICOLET 6700 FT-IR equipped with a commercial reaction chamber (Thermofisher) at the resolution of 1 cm $^{-1}$ . Ten scans were operated for each spectrum. Powder samples were purged in  $0.3\%~O_2/N_2$  balance from RT to 500~C. The sample cell was then cooled to 350~C under the same atmosphere.  $NO_x$  adsorption measurements were conducted by introducing freshly mixed  $0.075\%~NO/0.3\%~O_2/N_2$  balance to the chamber at 350~C. After the saturation of  $NO_x$  adsorption, which was judged by the invariant IR spectra, the sample was purged by  $N_2$  at 350~C till no changes happen to the IR spectra with the increasing time. The sample cell was subsequently heated to 500~C at 10~C/min, and  $NO_x$  desorption behaviors were recorded. The gas flow rate in all circumstances was 200~ml/min, and the tiny IR interference from gas molecules was subtracted.

In NSR activity tests, 0.5 g catalyst (0.2 g of 2 wt.% Pt/Al<sub>2</sub>O<sub>3</sub>) was mixed with quartz sand in a volume ratio of 1:3. The total flow rate is 1 L/min, with the space velocity of  $30,000 \, h^{-1}$ . A NICOLET 380 FT-IR equipped with a 2-m gas cell was used to detect the outlet concentrations of NO, NO<sub>2</sub>, NH<sub>3</sub>, N<sub>2</sub>O, CO, CO<sub>2</sub>, and H<sub>2</sub>O (g) at 4 s intervals. IR spectra of the multiple gases were collected at the same time. These spectra were automatically quantified by comparing them with the standardized spectra of diluted monocomponent gases at different concentrations, which were already set into mathematical functions as a method file. Home-developed software, OMINIC, TQ Analyst, and Macros Basic were connected to effectuate the calculations. A set of 1 min (lean)-1 min (rich) experiments and another set of 10 min (lean)-1 min (rich) experiments were conducted. The inlet gas concentrations are listed in Table 2. Calculations were made based on the reproducible concentration curves for at least 3 cycles (usually 5-6 cycles were required before stabilization). NO<sub>x</sub>-TPD experiments were conducted on the same equipment with the same flow rate. Powder samples were pre-treated in 7.5% O<sub>2</sub>/N<sub>2</sub> at 500 °C for 20 min, and

**Table 2** Inlet gas concentrations of 1 min (lean)–1 min (rich) NSR tests.

Gases	Concentrations (by volume	Concentrations (by volume <sup>a</sup> )			
	Lean periods	Rich periods			
NO	500 ppm	500 ppm			
02	7.5%	0			
CO	0	7.5%			
CO <sub>2</sub>	10%	10%			
H <sub>2</sub> O	10%	10%			
$N_2$	Balance	Balance			

<sup>&</sup>lt;sup>a</sup> NO injection was switched off in rich period of 10 min (lean)-1 min (rich) tests.

then cooled to 50 °C under  $N_2$  protection. The catalysts were saturated in 1.68% NO/7.5%  $O_2/N_2$ . After  $N_2$  purge, the samples were heated to 500 °C in  $N_2$  at 10 °C/min. NO and NO<sub>2</sub> were the only components detected by MCT detector and were having similar product distributions with the temperatures due to the same Pt/  $Al_2O_3$  part.

#### 3. Results

# 3.1. Chemical and physical evolutions during aging

The effect of 10% CO<sub>2</sub> hydrothermal 12 h aging was first investigated over the 30 wt.% Ba-supported samples. The *ex situ* XRD

patterns are shown in Fig. 1. Under this aging atmosphere, the formation of BaCeO<sub>3</sub> was not detected in either the 30 wt.% BaO/CeO<sub>2</sub> series (Fig. 1B) or the corresponding Pt-loaded samples (Fig. 1A). Peaks attributed to orthorhombic BaCO<sub>3</sub> (BaCO<sub>3</sub>-O) and CeO<sub>2</sub> grew sharper after aging, indicating larger crystallites were formed due to particle sintering during the aging. Pt particles (not detected by XRD because of the high dispersion or low loading ratio) in proximity to the barium species and the ceria did not stimulate Ba-CeO<sub>3</sub> formation. Only the crystal sizes of the particles were modified by Pt impregnation, because the BaCO<sub>3</sub> can be dissolved by Pt(NO<sub>3</sub>)<sub>2</sub> solution [20]. On the other hand, crystal decomposition of BaCO<sub>3</sub>-O occurred in the cases of Ba/Al (Fig. 1C) and Ba/Zr (Fig. 1D) series. This phenomenon was accompanied by the appearance of BaAl<sub>2</sub>O<sub>4</sub> and BaZrO<sub>3</sub>, which were also detected in the Ptloaded samples by other researchers [12,13]. Ceria materials resistance to the formation of BaCeO<sub>3</sub>, regardless of the NM locations. provides an advantage over the other two support oxides. The following work is going to focus on the specific effects of CO<sub>2</sub> and H<sub>2</sub>O during the aging treatments to Ba/Ce materials.

First, the capabilities of BaCeO<sub>3</sub> formation and decomposition were confirmed. The process of BaCeO<sub>3</sub> formation in BaCe11 during 0–18 h thermal aging in air and the regeneration of the 12 h thermal-aged sample in CO<sub>2</sub> are depicted by *in situ* XRD patterns in Fig. 2. After 12 h thermal aging, a significant amount of BaCeO<sub>3</sub> phase formed. This increasing trend continued through the thermal aging. In contrast, when a 10% CO<sub>2</sub> hydrothermal aging feed was introduced into the *in situ* reactor after 12 h thermal aging, the

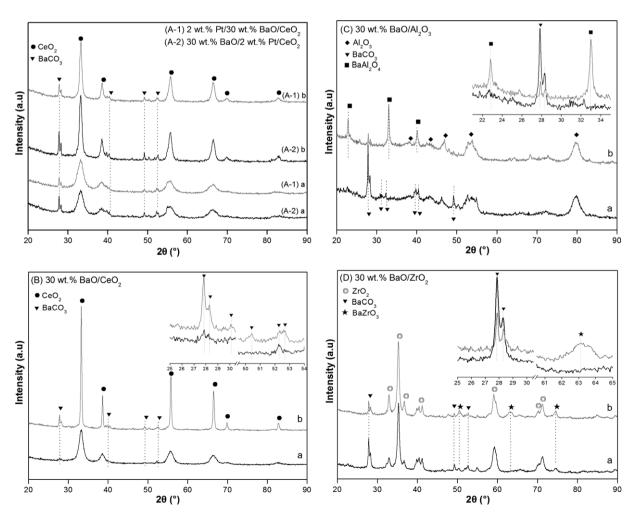
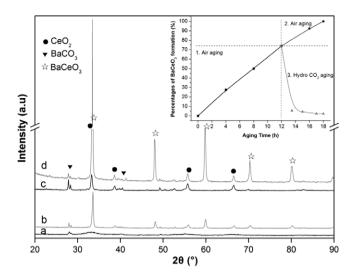
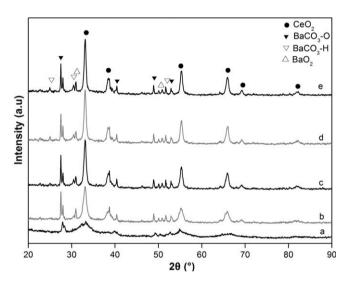


Fig. 1. XRD patterns of (a) fresh and (b) 10% CO<sub>2</sub> hydrothermal-aged samples with variant Pt loadings (A) or different support oxides (B–D). Part figures illustrate the major changes of crystallites between fresh (black) and aged (gray) samples in larger scales.



**Fig. 2.** *In situ* XRD patterns of (a) fresh, (b) 12 h thermal aged, (c) 6 h 10% CO<sub>2</sub> hydrothermal aged in addition to (b), and (d) 18 h thermal-aged BaCe11 compounds. Insert illustrates the progress in BaCeO<sub>3</sub> crystallization and decomposition (set the BaCeO<sub>3</sub> content in 18 h thermal-aged sample as 100%).



**Fig. 3.** In situ XRD patterns of BaCe11 compounds in their (a) fresh state (asprepared sample at RT) and aged in 5% CO<sub>2</sub> thermal condition for (b) 0 h (asprepared sample just reaching 800 °C), (c) 4 h, (d) 8 h, and (e) 12 h.

XRD peaks attributed to  $BaCeO_3$  disappeared and the peaks attributed to  $CeO_2$  and  $BaCO_3$  re-appeared, indicating that the regeneration of  $BaCeO_3$  to  $BaCO_3$ –O and  $CeO_2$  crystallites occurred. The percentage of  $BaCeO_3$  crystal formation (normalized to the crystal phase after 18 h thermal aging) was estimated based on the intensity of the diffraction features and is shown in the insert of Fig. 2.

Although the existence of amorphous particles cannot be discounted [12], the overall trend clearly demonstrates the poor chemical stability of BaCeO<sub>3</sub> in 10% CO<sub>2</sub> hydrothermal conditions. The reappearance of BaCO<sub>3</sub>–O and CeO<sub>2</sub> phases suggests that the balance between barium species and ceria has been shifted, and the formation of BaCO<sub>3</sub> and CeO<sub>2</sub> phases is favored over the formation of BaCeO<sub>3</sub> in the presence of 10% CO<sub>2</sub> and steam at 800 °C.

Second, the specific effects of CO<sub>2</sub> and steam in lean aging were studied separately. Fig. 3 presents the in situ XRD patterns for BaCe11 aged in a 5% CO<sub>2</sub> thermal condition. The results indicate that a CO<sub>2</sub> concentration as low as 5% is enough to suppress BaCeO<sub>3</sub> formation at 800 °C. Two new phases, hexagonal BaCO<sub>3</sub> (BaCO<sub>3</sub>-H) and BaO<sub>2</sub>, were detected. During the decarbonation, the phase transition of BaCO<sub>3</sub>-O to BaCO<sub>3</sub>-H occurs first [21]. Theoretical energy for the transformation from BaCO<sub>3</sub>-O  $(5.4 \times 9.0 \times 6.6 \text{ Å}^3,$ whiterite structure) to BaCO<sub>3</sub>-H (5.4  $\times$  5.4  $\times$  18.8 Å<sup>3</sup>, calcite structure) was estimated to be about 0.6 eV [22]. Hexagonal BaCO<sub>3</sub> has an intermediate stability and is of relevance to the start of NO<sub>x</sub> trapping [22]. Previous studies [23,24] have addressed the positive role of BaO<sub>2</sub> as a metastable species during LNT, where  $O_2^{2-}$  can be stabilized in BaO<sub>2</sub> lattice under oxidative atmosphere and at higher temperatures [23]. These phases are believed to be active but very unstable. They were not detected at ex situ RT and in situ conditions without CO<sub>2</sub> or with steam (discussed later). The presence of 5% CO<sub>2</sub> promotes the stability of barium carbonates during the polymorphic transformations and inhibits the migration of decomposed Ba<sup>2+</sup> and O<sup>2-</sup> to the ceria lattice to form BaCeO<sub>3</sub>. When using 10% CO2 thermal in situ-aged samples, similar results can be found with only minor differences in barium species distributions (summarized in Table 3).

TG-DSC results (Fig. 4) record several stages of decompositions and solid reactions under different atmospheres. Weight loss below 300 °C is related to the decomposition of amorphous carbonates, and the weight loss over 600 °C is attributed to the decomposition of bulk structured carbonates [12,18,19]. The samples heated in air showed drastic weight loss right above 750 °C (A and B). Whereas the samples heated in 5% CO<sub>2</sub> showed continuous slight weight loss without drastic drops until 1000 °C (C and D). In accordance with the theoretical analysis [25], 100% decomposition of BaCO<sub>3</sub> above 1100 °C is thermodynamically inevitable in all the conditions we investigated. However, based on the DSC curves, we still notice that the decomposition of BaCO<sub>3</sub> in air only conditions is apparently more endothermic than that in air  $+ CO_2$  conditions. Since BaCeO<sub>3</sub> formation at 800 °C has been well documented [11,12], it is safe to conclude that the rapid weight loss at 800 °C, accompanied with the more endothermic peaks, is caused by the decomposition of carbonates and the simultaneous promoted Ba-CeO<sub>3</sub> formation. Anyway, it is not guaranteed that all the BaCO<sub>3</sub> decomposed can form BaCeO<sub>3</sub> with CeO<sub>2</sub> within the limited time span in one TG experiment. The presence of 5% CO<sub>2</sub> suppresses the BaCeO<sub>3</sub> formation promoted decomposition of BaCO<sub>3</sub> around 800 °C. This phenomenon is clearer in BaCe11 samples at all heating rates (results not shown for 5 and 15 °C/min tests), where the two temperature regions of decompositions can be well defined

**Table 3**Percentages of detected Ba-based crystallites and particle sizes calculated based on *in situ* XRD patterns of BaCe11 compounds after 12 h aging treatments.

Aging treatments	Percentag	es of detected Ba-based crys	BaCeO <sub>3</sub> particle	Orthorhombic BaCO <sub>3</sub>		
	BaO <sub>2</sub>	Hexagonal BaCO <sub>3</sub>	Orthorhombic BaCO <sub>3</sub>	BaCeO <sub>3</sub>	sizes (Å)	particle sizes (Å)
Thermal	=	=	21	44	250 ± 15	na
Hydrothermal	-	_	5	72	352 ± 11	na
5% CO <sub>2</sub> thermal	14	16	25	-	_	106 ± 11
10% CO <sub>2</sub> thermal	14	14	30	_	-	117 ± 11
5% CO <sub>2</sub> hydrothermal	_	_	60	_	-	150 ± 15
10% CO <sub>2</sub> hydrothermal	-	-	76	-	-	190 ± 45

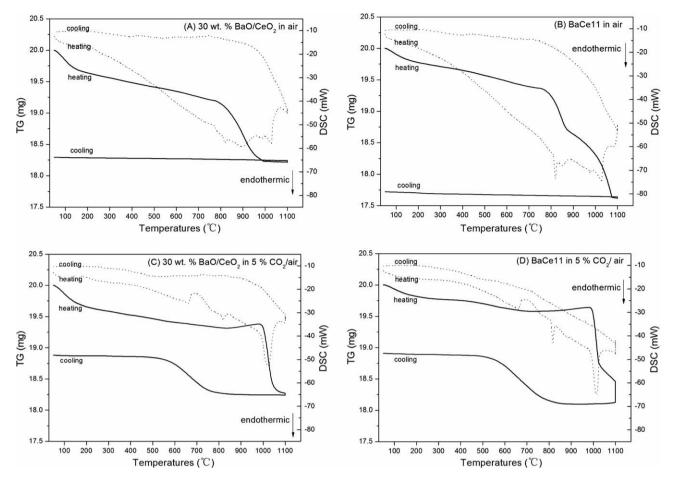


Fig. 4. TG (black) and DSC (gray dashed) curves of the samples heated from 50 to 1100 °C at the rate of 10 °C/min, stabilized at 1100 °C for 20 min, and cooled back at the rate of -10 °C/min in air (A and B) air, and 5%  $CO_2/air$  (C and D).

with the narrow endothermic DSC peaks located at 800 (minor) and  $1000\,^{\circ}\text{C}$  (major), corresponding to the idealized pure decarbonation process [25], and the interference of CeO<sub>2</sub> support oxide should be very limited even at  $1100\,^{\circ}\text{C}$  due to the barrier for BaCeO<sub>3</sub> formation. According to the method proposed by Tomashevitch et al. [26], we assume a kinetics equation for the decomposition reaction:

$$\frac{\partial \alpha}{\partial \tau} = k_0 \exp\left(-\frac{E_A}{RT}\right) f(\alpha) \tag{1}$$

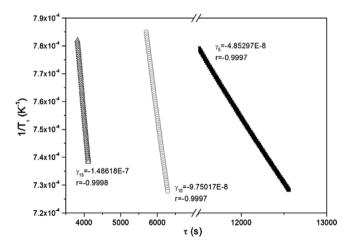
 $\alpha$  is the degree of conversion,  $k_0$  the pre-exponential factor,  $E_A$  the activation energy, and  $f(\alpha)$  the temperature independent kinetic function. At high temperatures, the reciprocal temperature growth is almost a linear function of time (Fig. 5):

$$\frac{1}{T(\tau)} = \frac{1}{T_0} + \gamma T \tag{2}$$

Eq. (1) can thus be integrated, and the activation energy  $E_A$  can be obtained from at least two experiments with different  $\gamma_i$ , without any assumptions of functional form of  $f(\alpha)$ :

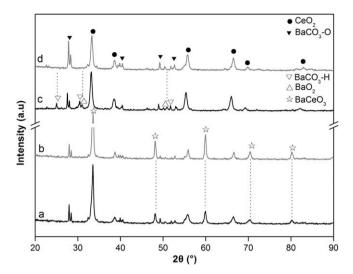
$$\begin{split} \frac{1}{\gamma_{5}} \left\{ 1 - \exp\left(-\frac{E_{A}\gamma_{5}\tau}{R}\right) \right\} &= \frac{1}{\gamma_{10}} \left\{ -\exp\left(-\frac{E_{A}\gamma_{10}\tau}{R}\right) \right\} \\ &= \frac{1}{\gamma_{15}} \left\{ 1 - \exp\left(-\frac{E_{A}\gamma_{15}\tau}{R}\right) \right\} \end{split} \tag{3}$$

It is observed that in air flow, the activation energy of BaCO<sub>3</sub> decomposition is  $145 \pm 25$  kJ/mol around 800 °C (promoted by ceria contact) and  $250 \pm 17$  kJ/mol above 1000 °C. Whereas the  $E_A$  is as high as  $500 \pm 17$  kJ/mol for CO<sub>2</sub> protected samples throughout the



**Fig. 5.** Reciprocal heating rate constants  $\gamma_5$ ,  $\gamma_{10}$ , and  $\gamma_{15}$  corresponding to the heating rates of 5, 10, and 15 °C/min, respectively. When the percentages of BaCO<sub>3</sub> decomposition ( $\alpha$ ) are in the range of 20–90%, reaction time ( $\tau$ ) was big enough to guarantee the hyperbolic temperature–time curves be fitted in linear way.

heating process. This is similar with the theoretical calculation results [27], predicting an almost one time higher  $E_A$  is required for BaCO<sub>3</sub> decomposition in CO<sub>2</sub> contained flows, invariant with CO<sub>2</sub> partial pressures. When the temperatures were decreased to 800 °C from 1100 °C, the regaining of weight happened on the samples treated in 5% CO<sub>2</sub>/air flow, indicating the chemical balance is moving toward the carbonates formation again.



**Fig. 6.** *In situ* XRD patterns of BaCe11 compounds treated for 12 h in (a) thermal, (b) hydrothermal, (c) 10% CO<sub>2</sub> thermal, and (d) 10% CO<sub>2</sub> hydrothermal conditions.

The effects of steam are more morphological than chemical. For the in situ XRD patterns in Fig. 6, the difference mainly involves the crystallinity of different compositions, and the overall chemical equilibrium between barium species and ceria species is still dominated by CO2. In the cases of thermal aging and hydrothermal aging, BaCeO<sub>3</sub> was detected. In the presence of 10% steam, changes in crystallites are more pronounced than the thermally aged sample. A more noticeable increase in BaCeO<sub>3</sub> crystallinity is accompanied by a significant decrease in CeO2 and BaCO3-O XRD peaks. However, this does not necessarily imply that steam inhibits the stabilization carbonates in the presence of CO<sub>2</sub>. During the aging processes when 10% CO<sub>2</sub> was present, the formation of BaCeO<sub>3</sub> was absent regardless of the presence of steam. For the 10% CO<sub>2</sub> hydrothermal-aged sample (Fig. 6d), the crystallite growth of BaCO<sub>3</sub>-O is higher than that of the 10% CO<sub>2</sub> thermal-aged sample (Fig. 6c). Furthermore, in situ XRD patterns in Fig. 6d show no evidence of BaO<sub>2</sub> and BaCO<sub>3</sub>-H crystal's existence. Therefore, regardless of CO<sub>2</sub> existence, steam in the aging atmosphere seems to serve only as a promoter for the crystal growth of the most stable ceria and barium phases in certain aging conditions.

The percentages of crystalline barium phases [12] and their crystal sizes are calculated based on XRD patterns (Table 3). The particle sizes of  $BaCO_3$ –H and  $BaO_2$  are unable to be calculated because of their scattered weak peaks. In sum,  $BaCO_3$ ,  $BaO_2$ ,  $CeO_2$ ,  $Ba-CeO_3$  can coexist in aging conditions. Under the protection of  $CO_2$ , orthorhombic  $BaCO_3$  and  $CeO_2$  are the most stable components below  $800\,^{\circ}$ C. Steam accelerates the morphological changes, but it does not determine the above chemical equilibrium. Larger crystal sizes of the thermodynamic favored stable phases can be detected in the presence of steam and higher concentrations of  $CO_2$ .

The changes of surface areas during the aging are listed in Table 4. For both BaCe11 and 30 wt.% BaO/CeO<sub>2</sub> samples, the trends of the surface areas' changes are similar. In the absence of CO<sub>2</sub>, more significant decrease in surface areas is observed. Although the decomposition of barium carbonates before the formation of BaCeO<sub>3</sub> crystallites may contribute to the increase in surface area [28], this effect was not observable here. The surface areas of the samples aged in CO<sub>2</sub> are generally higher, especially for those samples aged in lower concentrations of CO<sub>2</sub>. The presence of steam in the aging atmosphere results in lower surface areas. In comparison with BaCe11 compounds, 30 wt.% BaO/CeO<sub>2</sub> samples with higher initial surface areas suffered the more obvious surface areas declines after aging. Because of the significant sintering effect, even with similar distribution of chemical components, the catalytic

Table 4
Surface areas of BaCe11 and 30 wt.% BaO/CeO<sub>2</sub> after 12 h different aging treatments.

Aging treatments	$S_{\rm BET}^{a}$ (m <sup>2</sup>	$S_{\rm BET}^{\ a}$ (m <sup>2</sup> /g) and decreasing percentages				
	BaCe11	BaCe11		BaO/CeO <sub>2</sub>		
Thermal	9.7	50.5%	18.7	77.4%		
Hydrothermal	7.9	59.7%	10.0	88.0%		
5% CO <sub>2</sub> thermal	11.4	41.8%	31.8	61.6%		
10% CO <sub>2</sub> thermal	10.7	45.4%	31.1	62.5%		
5% CO <sub>2</sub> hydrothermal	10.7	45.4%	23.9	71.2%		
10% CO <sub>2</sub> hydrothermal	10.8	44.9%	22.4	73.0%		

 $<sup>^{\</sup>rm a}$   $S_{\rm BET}$  of the fresh BaCe11 and 30 wt.% BaO/CeO $_{\rm 2}$  are 19.6 and 83.0  $\rm m^2/g,$  respectively.

activity of 30 wt.%  $BaO/CeO_2$  inevitably decreases along the increasing aging times (activity data not shown for brevity). SEM images of 30 wt.%  $BaO/CeO_2$  samples illustrated in Fig. 7 further confirm the influences of different aging conditions. In the absence of  $CO_2$ , formation of  $BaCeO_3$  (light color) in downy shape takes place, and the spherical structures of 30 wt.%  $BaO/CeO_2$  are destroyed severely. The presence of  $CO_2$  not only suppresses  $BaCeO_3$  formation, but also manages to maintain the original morphologies of the catalysts to some extent. Among all the cases we investigated, the introduction of water promotes the aggregation of the particles.

# 3.2. Catalytic activity changes induced by aging

Different aging treatments have brought about significant influences on NO<sub>x</sub> adsorption and desorption behaviors in NSR reactions. Referred to the recent literatures [29-31], specific assignments of the IR bands are labeled in Figs. 8 and 9. The designations Al, Ce, and Ba suggest the surfaces where adsorbates are bonded. During NO<sub>x</sub> adsorption (Fig. 8), bands attributed to bridged nitrate on Al<sub>2</sub>O<sub>3</sub> were found around 1240 cm<sup>-1</sup>, chelating nitrate on Al<sub>2</sub>O<sub>3</sub> at 1570 cm<sup>-1</sup>, nitrate on CeO<sub>2</sub> at 1535 cm<sup>-1</sup>, NO<sub>2</sub><sup> $\delta$ +</sup> on CeO<sub>2</sub> around 1780–1760 cm<sup>-1</sup>, monodentate nitrate associated with BaO around 1291 cm<sup>-1</sup>, and ionic nitrate associated with BaO around 1360-1350 cm<sup>-1</sup>. The order of these bands introduced is in line with their stability from low to high. The major bands of ionic nitrate associated with BaO and minor bands of nitrate on CeO2 were able to be maintained after N<sub>2</sub> purge (Fig. 9). Formation of nitrite was not detected in the experiments because of the high reaction temperature, and the pre-adsorption of water and oxygen on catalysts' surface during aging can be excluded by the pre-treatment.

After mixing 30 wt.% BaO/CeO<sub>2</sub> with 2 wt.% Pt/Al<sub>2</sub>O<sub>3</sub>, the adsorption behaviors of the catalysts are very different from pure 2 wt.% Pt/Al<sub>2</sub>O<sub>3</sub> (almost no adsorption after N<sub>2</sub> purge), indicating the main storage function of BaO/CeO<sub>2</sub> part. The bands of ionic nitrate appear after the evolution of other increasing nitrate bands. The maintenance of these bands after N<sub>2</sub> purge (Fig. 9) indicates their higher stability, and the stabilization of these nitrate species should be closely related to the activity on the major NO<sub>x</sub> storage sites [29]. Adsorptions over fresh catalyst show the highest IR intensity, whereas the samples with increasing amount of BaCeO<sub>3</sub> formation or/and higher level of crystallinity (either BaCeO3 or BaCO<sub>3</sub>) suffered the decrease in adsorption intensity, especially on barium and ceria sites The deactivations of BaO/CeO2 parts during aging are not only indicated by the weaker IR intensity, but the distributions of their IR signals appear to be more similar to those of Pt/Al<sub>2</sub>O<sub>3</sub>. Fine active phases, including BaCO<sub>3</sub>-O, BaCO<sub>3</sub>-H, and BaO<sub>2</sub> which are inclined to be maintained in CO<sub>2</sub>, are believed to benefit the NO<sub>x</sub> storage amount and rate and to facilitate the major trapping capacity on BaO/CeO<sub>2</sub>.

At the beginning of the desorption, little evidence of nitrate/nitrite adsorption can be observed on 2 wt.% Pt/Al<sub>2</sub>O<sub>3</sub> sample (Fig. 9),

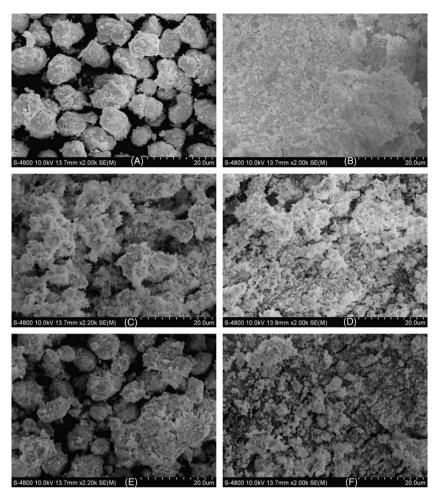


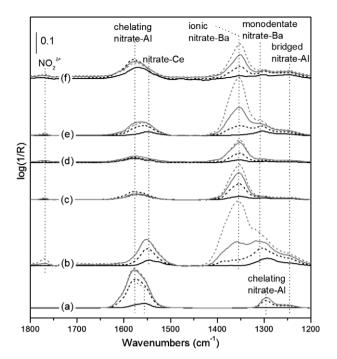
Fig. 7. SEM images of 30 wt.% BaO/CeO<sub>2</sub> in (A) fresh state, and treated in (B) 1100 °C calcinations in air for 4 h, (C) thermal, (D) hydrothermal, (E) 10% CO<sub>2</sub> thermal, and (F) 10% CO<sub>2</sub> hydrothermal aging conditions.

indicating the negligible stable NO<sub>x</sub> storage capacity of Pt/Al<sub>2</sub>O<sub>3</sub> at 350 °C. Moreover, the initial difference among the other five spectra (NO<sub>x</sub> saturated) at 350 °C is not as significant as that in the previous adsorption measurements with time limit, indicating the increasing crystallinity or/and BaCeO3 formation not only decreases the amount of active sites, but can hinder the  $NO_x$  trapping rate. For thermal and hydrothermal-aged samples, limited amount of nitrate bonds dissociated below 400-450 °C, but the NO<sub>x</sub> desorption is greatly accelerated right above 450 °C. In contrast, IR bands of nitrate over fresh and CO<sub>2</sub>-aged samples decreases in a milder manner with the increasing temperatures, and higher amount of surface nitrate adsorbates has been released in every temperature range. Monodentate nitrate, having lower thermal stability than ionic nitrate, reappears above 400 °C. These stabilizing effects to metastable adsorbates remind us the above in situ XRD observations of multiple BaCO<sub>3</sub> phases and BaO<sub>2</sub> in CO<sub>2</sub> without steam. In the N<sub>2</sub> flow, the existence of metastable phases and oxidative sites provides intermediate nitrate species a higher possibility to be stabilized on catalysts' surface.

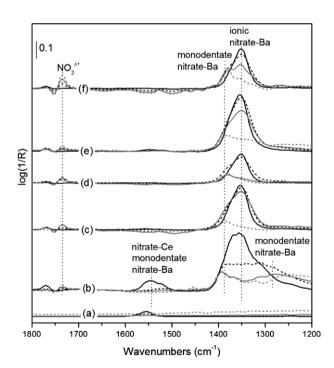
 $NO_x$ -TPD result (Fig. 10) also shows that  $Pt/Al_2O_3$  has limited  $NO_x$  trapping capability, when compared with that of  $BaO/CeO_2$  part. The saturated amount of adsorbed  $NO_x$  of the aged samples is obviously different. But it is not as significant as that in the  $in\ situ$  adsorption process with time limit, in which the trapping rates are going to make larger differences. As revealed by the data,  $BaCeO_3$  formation still weighs the worst for  $NO_x$  trapping, and the higher crystallinity of  $BaCO_3$  induced by coexistence of steam and  $CO_2$  shows minor negative role for the overall  $NO_x$  trapping capac-

ity. As the DRIFTS results indicated,  $NO_x$  adsorption on Ce sites has very poor stability under  $N_2$  purge at 350 °C. Therefore,  $NO_x$  sorption on active ceria sites can only contribute to low temperature adsorptions, and the  $NO_x$  desorption peaks above 350 °C should be mainly related to the activity of barium sites, pertaining to barium nitrate decomposition. In accordance with the DRIFTS results (Fig. 9), the thermal and hydrothermal-aged samples not only show the weakest desorption intensity, but their desorption processes quickly completed around 400-450 °C. For the  $CO_2$ -aged samples, neither BaCeO<sub>3</sub> formation nor the most severe sintering happens, and the  $NO_x$  desorption above 400 °C is still noticeable and is only less than that of the fresh catalyst. The higher crystallinity of carbonates and the aggregation of support oxides, especially when steam and  $CO_2$  exist, are the contributing factors for the decline.

Catalytic performances of 2 wt.% Pt/Al<sub>2</sub>O<sub>3</sub> + 30 wt.% BaO/CeO<sub>2</sub> catalysts were evaluated at 350 °C, where the NO oxidation over Pt/Al<sub>2</sub>O<sub>3</sub> is not the rate controlling step, and the aging effects on barium species should be more obvious. Exposure in a lean period for 10 min is sufficient for the samples to approach the NO<sub>x</sub> saturated stage. Table 5 lists the key data of the evaluations. Samples containing BaCeO<sub>3</sub> (after thermal and hydrothermal aging treatments) suffered the greatest activity decrease in comparison with the fresh catalyst. To another extreme, without BaCeO<sub>3</sub> formation, samples aged under high concentrations of CO<sub>2</sub> and steam also suffered an obvious but minor decrease in NSC. During the rich period, NO was switched off, and only the NO<sub>x</sub> released from the storage sites participated in the reduction process. It is observed that

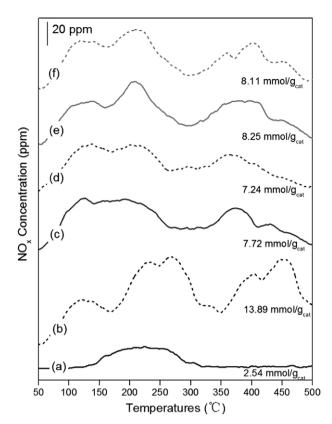


**Fig. 8.** In situ DRIFTS spectra recorded at 5 (black), 10 (black dashed), 15 (gray), and 20 (gray dashed) min during  $NO_x$  adsorption at 350 °C on (a) 2 wt.%  $Pt/Al_2O_3$ , and 2 wt.%  $Pt/Al_2O_3 + 30$  wt.%  $BaO/CeO_2$  catalysts in (b) fresh, (c) thermal, (d) hydrothermal, (e) 10%  $CO_2$  thermal aged, (f) 10%  $CO_2$  hydrothermal states.



**Fig. 9.** *In situ* DRIFTS spectra recorded at 350 (black), 400 (black dashed), 450 (gray), and 500 (gray dashed)  $^{\circ}$ C during NO<sub>x</sub> adsorption from 350 to 500  $^{\circ}$ C at the heating rate of 10  $^{\circ}$ C/min on (a) 2 wt.% Pt/Al<sub>2</sub>O<sub>3</sub>, and 2 wt.% Pt/Al<sub>2</sub>O<sub>3</sub> + 30 wt.% BaO/CeO<sub>2</sub> catalysts in (b) fresh, (c) thermal, (d) hydrothermal, (e) 10% CO<sub>2</sub> thermal aged, (f) 10% CO<sub>2</sub> hydrothermal states.

catalysts with a higher NSC generally release a higher amount of  $NH_3$  and a lower fraction of unreduced NO during the rich periods, compared with the amount of  $NO_x$  trapped during the lean periods. Reducing agent should be excessive in such a case, and higher crystallinity of the materials after aging inhibits the efficient  $NO_x$  release and reduction.



**Fig. 10.** NO<sub>x</sub>-TPD profiles of (a) 2 wt.% Pt/Al<sub>2</sub>O<sub>3</sub> (0.2 g), and 2 wt.% Pt/Al<sub>2</sub>O<sub>3</sub> (0.2 g) + 30 wt.% BaO/CeO<sub>2</sub> (0.3 g) catalysts in (b) fresh, (c) thermal, (d) hydrothermal, (e) 10% CO<sub>2</sub> thermal aged, (f) 10% CO<sub>2</sub> hydrothermal states. Total amount of NO<sub>x</sub> desorbed is labeled beside the curves.

Another set of tests was conducted in 1 min–1 min lean–rich cycles with non-stopping NO injections during rich periods. Fig. 11 illustrates the periodic evolution of NO, NO<sub>2</sub>, N<sub>2</sub>O, NH<sub>3</sub>, CO, CO<sub>2</sub>, and H<sub>2</sub>O concentrations. H<sub>2</sub> and CO coexisted during the rich periods because of the WGS reaction. The NH<sub>3</sub> "tail" was observed at the beginning of lean period. Because NH<sub>3</sub> is a "sticky" gas in the reactor sampling lines, the lag from the NH<sub>3</sub> signal in the FT-IR analysis becomes possible [32]. Besides the NO breakthrough during the rich periods, N<sub>2</sub>O release was also detected, but it became less noticeable when the temperature increased.

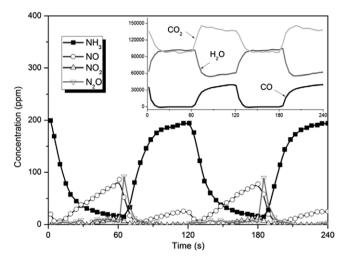
Not only the formation of sintered BaCeO<sub>3</sub> does, but the increased crystallinity of carbonates has a negative effect on the rapid storage and complete release of NO<sub>x</sub>. The concentrations of NO, NO<sub>2</sub>, and NH<sub>3</sub> at 350 °C are shown in Fig. 12. The amount of NO<sub>x</sub> stored during the 1 min lean period was compared with the saturated amount of NO<sub>x</sub> after 10 min (Table 5). The aged samples without the formation of BaCeO<sub>3</sub> show higher NO<sub>x</sub> trapping capacities and rates. But if the samples were aged in higher concentrations of CO2 and steam, their advantages have been weakened. For the samples that show higher NSC during the lean periods, the corresponding amounts of NOx and NH3 released during the rich periods are less. The NH<sub>3</sub> formed in the forefront of catalysts' bed during rich conditions can further react with the injected and released NO through the catalysts, especially when residual oxygen in gas phase or ceria lattice oxygen can participate in the favorable NH<sub>3</sub>-NO-O<sub>2</sub> reduction [33-35]. Due to the oxygen storage capacity (OSC) of CeO<sub>2</sub>, the ceria lattice may supply oxygen to participate in the NO<sub>x</sub> reduction [36]. To further confirm this, we used 4% CO/N<sub>2</sub> and  $2\% O_2/N_2$  as the 1 min rich and lean atmospheres, respectively, between which a 1 min N<sub>2</sub> purge was applied. The OSC activity was evaluated based on the amount of CO<sub>2</sub> produced in rich periods (Table 5). The CO<sub>2</sub> production of all samples in lean periods is

Table 5
Performances of the 2 wt.% Pt/Al<sub>2</sub>O<sub>3</sub> + 30 wt.% BaO/CeO<sub>2</sub> catalysts prepared using different aging treatments during 10 min (lean)–1 min (rich) NSR cycles at 350 °C.

Samples	Lean $NO_x$ stored ( $\mu mol/g_{cat}$ ) and percentages of $NO_x$ stored in 1 min		Rich $NH_3$ released ( $\mu mol/g_{cat}$ ) and percentages to $NO_x$ stored in 10 min		Rich $NO_x$ released ( $\mu mol/g_{cat}$ ) and percentages to $NO_x$ stored in 10 min		OSC in 1 min rich period (µmol/g <sub>cat</sub> )
Fresh	67.0	99.9%	36.2	54.0%	5.6	8.4%	213.6
Thermal	46.1	87.0%	35.0	75.9%	8.9	21.8%	167.9
Hydrothermal	40.9	78.0%	27.3	66.7%	10.7	23.2%	156.7
5% CO <sub>2</sub> thermal	60.3	82.9%	39.0	64.7%	5.3	8.8%	195.8
10% CO <sub>2</sub> thermal	58.8	78.0%	35.8	61.0%	7.1	12.1%	195.0
5% CO <sub>2</sub> hydrothermal	56.5	78.2%	32.1	56.7%	8.7	15.4%	189.2
10% CO <sub>2</sub> hydrothermal	55.8	78.3%	28.3	50.7%	9.2	16.5%	186.1

<sup>\*</sup> The 1 min NSCs for 2 wt.% Pt/30 wt.% BaO/CeO<sub>2</sub> samples are 103.0 μmol/g<sub>cat</sub> (fresh) and 87.5 μmol/g<sub>cat</sub> (10% CO<sub>2</sub> hydrothermal).

<sup>\*</sup> The 1 min NSC for fresh 2 wt.%  $Pt/Al_2O_3$  is 14.6  $\mu$ mol/ $g_{cat}$ .



**Fig. 11.** 1 min (lean)–1 min (rich) NSR reaction profiles of NH<sub>3</sub>, NO, NO<sub>2</sub>, and N<sub>2</sub>O at 300  $^{\circ}$ C. Insert illustrates the periodic changes of CO, CO<sub>2</sub>, and steam concentrations.

around 90-100 μmol/g<sub>cat</sub>, which is related to the similar CO adsorptions in the previous rich period [37]. Generally, ceria-based catalysts that suffer less extent of thermal deterioration produce higher amount of OSC in rich conditions, and the trace amount of oxygen species released from ceria seems to have positive correlation with N<sub>2</sub> selectivity. However, we are reserved to claim that higher OSC should be desirable for lean NO<sub>x</sub> storage. According to the concentration curves (Fig. 12), we observed that the  $NO_x$  concentration in lean period keeps going down for 50 ppm in 20 s for the fresh sample at 350 °C, but this did not happen for other aged samples with lower OSC. Since the same Pt/Al<sub>2</sub>O<sub>3</sub> part for NO oxidation has been applied, the states of fresh ceria should be the main contributing factor here. It is inferred that this hindering effect of NO<sub>x</sub> trapping at the very beginning of the lean period is due to the higher amount of Ce3+ formed and residual reducing agent adsorbed on ceria surface after the pervious rich period [37,38]. If the OSC activity is lower, which means the  $CeO_2$  support oxides have less Ce<sup>3+</sup> and be more oxidative, NO<sub>x</sub> should be stored and stabilized more easily at the beginning of the lean period. In such a sense, higher OSC is not desirable in our specific conditions.

# 4. Discussion

# 4.1. Effect of CO<sub>2</sub> in lean aging

In terms of materials' activity, we find that, to some extent, the presence of  $CO_2$  has a positive effect in maintaining the  $NO_X$  trapping sites in barium species. Without  $CO_2$  during high temperature

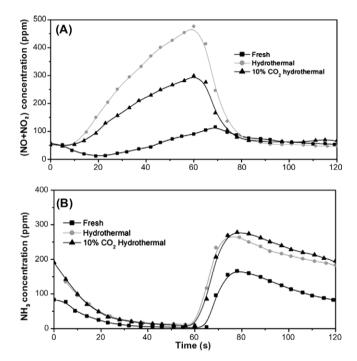


Fig. 12. NSR response curves at 350 °C for (A) NO + NO $_2$  and (B) NH $_3$  during a complete lean–rich cycle with different 2 wt.% Pt/Al $_2$ O $_3$  + 30 wt.% BaO/CeO $_2$  catalysts.

aging, BaCO<sub>3</sub> can easily decompose into BaO and form BaCeO<sub>3</sub> with CeO<sub>2</sub> at 800–850 °C. The solid reaction between the Ba–Ce phases on catalysts' interfaces diminishes large quantity of NO<sub>x</sub> trapping sites for stable nitrate formation. Moreover, as the two phases almost crashed into the lattice of each other during BaCeO<sub>3</sub> formation, the accompanied severe sintering of the catalysts greatly decreases the nitrate' stability. Fortunately, as little as 5% CO2 hinders the formation of BaCeO<sub>3</sub> to even 1000 °C hydrothermal aging and improve the overall performance. Since CO<sub>2</sub> is present in leanburn exhaust with a normal concentration around 10%, the driving force of Ba/Ce catalysts' deactivation has been reconsidered in the present work. Low concentrations of CO<sub>2</sub> in aging atmosphere manage to maintain the chemical equilibrium among BaCO<sub>3</sub>, BaO, BaO<sub>2</sub>, Ba(OH)<sub>2</sub>, and CeO<sub>2</sub>. Because the thermodynamic equilibrium to BaCeO<sub>3</sub> formation is not favored in such circumstances, decarbonation of BaCO<sub>3</sub> particles in close contact with CeO<sub>2</sub> shows no significant difference to that of pure BaCO<sub>3</sub> [27]. The competition of CO<sub>2</sub> with NO<sub>x</sub> for barium sites has been reported to be negative in NSR reactions [5,36]. However, when low concentrations of CO<sub>2</sub> in the exhaust manage to avoid BaCeO<sub>3</sub> formation, and to maintain the metastable phases (BaCO<sub>3</sub>-H and BaO<sub>2</sub>) as fine particles, the

<sup>\*</sup> The 1 min NSCs for 30 wt.% BaO/2 wt.% Pt/CeO<sub>2</sub> samples are 94.7 µmol/g<sub>cat</sub> (fresh) and 78.3 µmol/g<sub>cat</sub> (10% CO<sub>2</sub> hydrothermal).

abundant nitrate in stable bonding with barium surface and efficient diffusion in bulk structure are less hindered by the high temperature treatment. Therefore, their dynamic NSR activity becomes more desirable among the aged samples.

# 4.2. Effect of steam in lean aging

Steam promotes the crystal growth of stable phases in thermodynamics during the aging. The inferior NO<sub>x</sub> storage and reduction efficiency on bulk structures of barium species have been documented in many works [16,35]. Water-induced morphological modifications over barium-based materials have been recently performed [39], and the effects of steam on the formation of bulk structured nitrate were corroborated. In our case, the effects of steam in lean aging mainly involve accelerating the aggregation of particles. In the absence of CO<sub>2</sub>, the presence of steam further promotes both the crystallization of BaCeO<sub>3</sub> and the decomposition of BaCO<sub>3</sub>. While with CO<sub>2</sub> to inhibit the formation of BaCeO<sub>3</sub>, steam promotes the crystallization of BaCO<sub>3</sub>-O, thus eliminating the intermediate phases such as BaCO<sub>3</sub>-H and BaO<sub>2</sub>. Whenever steam was present during the aging process, more severe sintering was observed. For NSR activities, concentration of steam shows a minor influence when compared with that of CO<sub>2</sub>, because it does not stimulate any new deactivating chemical reactions during the aging. Formation of BaCeO<sub>3</sub> is more detrimental than the higher crystallinity to efficient NSR cycles.

# 4.3. Deterioration of Ba/Ce-based NSR catalysts in lean-burn condition

The presence of CO<sub>2</sub> and steam during lean aging treatments induces obvious morphological and chemical changes to the Ba/Cebased NSR catalysts, and thus significantly modifies the catalytic performances. No matter if NM particles are in close contact with BaO/CeO<sub>2</sub> or not, the Ba-support interactions determine the composition and morphology of the barium components during the aging treatments. However, according to the NSR activity (fresh and aged) of 2 wt.% Pt/30 wt.% BaO/CeO<sub>2</sub> and 30 wt.% BaO/2 wt.% Pt/CeO<sub>2</sub> samples listed in Table 5, it is safe to conclude that the difference in percentile is weakened when fresh Pt is added directly to BaO/CeO<sub>2</sub> in our experimental conditions. Close Pt-Ba contact, which benefits NO<sub>x</sub> spilling over to barium storage sites [14], is the main reason that increases the NSC of Pt added samples. On the other hand, for the samples with direct Pt-Ce contact, NO oxidation activity can be decreased to some extent, due to the surface basicity [40]. Moreover, the Pt particles fully oxidized by ceria lattice oxygen may gradually become deactivated for lean NO<sub>x</sub> reduction and even oxidation [37,41]. In this sense, the addition of Pt makes the situation even complicated, especially when the aging treatments are going to significantly modify the morphologies and compositions of ceria-based components. Having very limited NO<sub>x</sub> trapping capacity, fresh Pt/Al<sub>2</sub>O<sub>3</sub> is applied in all the test conditions. By using such a catalyst' formulation, we expected to exclude the influence of different NO oxidation activity from Pt sites, and thus more precisely describe the changes and aging mechanisms in Ba-Ce interactions.

In the aging exhaust containing  $CO_2$ , the formation of  $BaCeO_3$  is thermodynamically suppressed, and the activity decline due to the particle aggregations of  $BaO/CeO_2$  materials needs more consideration. In order to obtain higher activity,  $NO_x$ , oxidized on the Pt sites, is expected to migrate quickly to the storage sites and transform into stable nitrate in lean conditions. In rich periods, the stored nitrate should be easily decomposed into  $NO_x$  for reduction. Being promoted by steam, higher concentrations of  $CO_2$  break the equilibrium among  $BaCO_3$ –O,  $BaCO_3$ –H, and  $BaO_2$ . Not only is the formation of  $BaCeO_3$ , which consumes carbonates and induces severe sintering, being suppressed, but the aging causes more barium

species to stabilize into bulk structured BaCO3-O and sintered CeO<sub>2</sub>. Larger barium particles create extra diffusion barriers for the formation/release of a large quantity of nitrite/nitrate in barium particles. Moreover, the stability of the weakly bonded nitrite and nitrate adsorbates can be drastically decreased by lowering the partial pressure of oxygen and favoring the exothermic reduction [42]. Because of the weak bonding with barium surfaces, nitrite/nitrate in larger barium particles rapidly decompose when encountering rich atmosphere or extra reaction heat. Much unreduced NO left the catalysts' bed in such conditions. Therefore, a decrease in NO<sub>x</sub> reduction efficiency was observed, even though the total amount of trapped NO<sub>x</sub> is less compared with the samples having better NSC. Milder NO<sub>x</sub> release during the rich periods allows sufficient gas-solid contact for the released NO<sub>x</sub> to be reduced into N<sub>2</sub> or NH<sub>3</sub> by Pt-catalysts. The NH<sub>3</sub> can then react with the NO in the adjacent zones of the catalyst bed to produce N<sub>2</sub> [34.35]. The formation of NH<sub>2</sub> is positively correlated with the efficient regeneration of NSC during the rich periods. A passive SCR catalyst following the NSR catalyst would be a beneficial utilization of the released NH<sub>3</sub>. The lattice oxygen released by ceria may improve  $NO_x$  reduction by increasing  $N_2$  selectivity [36,43]. But the higher Ce<sup>3+</sup> content in reduced CeO<sub>2</sub> may destabilize the nitrate/nitrite formation on the catalysts surface at the beginning of the lean periods. OSC activity is in positive relationship with the less extent of sintering of CeO<sub>2</sub> support oxides, but it does not always guarantee the better NSR efficiencies. However, situations may be different when different lean-rich cycle lengths, gas concentrations, and ceria contents were applied [44,45].

#### 5. Conclusions

Because CO<sub>2</sub> and steam are present in lean-burn exhaust with percentages of about 10% in volume, their effects on the morphological and chemical properties of Ba-based NSR catalysts during aging treatments should be noted. The formation of BaAl<sub>2</sub>O<sub>4</sub> and BaZrO<sub>3</sub> over Ba/Al and Ba/Zr systems, respectively, can be detected after 800 °C 10% CO<sub>2</sub> hydrothermal aging for 12 h. However, in Ba/ Ce-based catalysts, CO<sub>2</sub> concentration as low as 5% (air balanced) can sufficiently suppress the formation of BaCeO<sub>3</sub> or decompose the pre-existing BaCeO<sub>3</sub> easily. Active and metastable NO<sub>x</sub> trap phases, such as hexagonal BaCO<sub>3</sub> and BaO<sub>2</sub>, are able to be maintained because of the chemical equilibrium established by low concentrations of CO<sub>2</sub>. During the decarbonation of BaCO<sub>3</sub> on CeO<sub>2</sub>, CO<sub>2</sub> raises its activation energy to the level of pure BaCO<sub>3</sub> crystallites, and thus sets off the promoting effect of CeO<sub>2</sub> support oxide in accelerating the decarbonation by forming Ba-Ce compounds. However, when more CO<sub>2</sub> and steam are injected, the chemical equilibrium moves toward further stabilization of the storage components. Many original NO<sub>x</sub> trapping phases in fresh samples transform into bulk structured BaCO3 and CeO2. The diffusion barriers for nitrate in bulk structure and the weak nitrite/nitrate bonding on catalysts' surface inhibit the efficient NO<sub>x</sub> sorption and mild release. For Ba-based NSR catalysts developed for better performance after aging, the effects of CO<sub>2</sub> and steam in the aging atmosphere should be thoroughly considered since they are key agents in modifying the morphology and chemistry of the catalysts.

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